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# Journal of Alloys and Compounds

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# Phase equilibria of the Cu-Ni-Si system at 700 °C

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### ARTICLE INFO

Article history:
Received 7 March 2011
Received in revised form 7 July 2011
Accepted 30 July 2011
Available online 4 August 2011

Keywords: Cu-Ni-Si system Phase diagram X-ray diffraction Electron probe microanalysis

### ABSTRACT

The phase equilibria at the isothermal section of the Cu–Ni–Si system at  $700\,^{\circ}\text{C}$  were experimentally investigated. Thirty Cu–Ni–Si alloys were prepared by arc melting and annealed at  $700\,^{\circ}\text{C}$  for 30 or 80 days, and examined with optical microscopy, X-ray diffraction, scanning electron microscopy with energy dispersive X-ray spectroscopy and electron probe microanalysis. Twelve three-phase regions were determined. The existence of the ternary compound  $\tau_1$ -Cu<sub>56.8-63</sub> Ni<sub>10.4-16.1</sub> Si<sub>26.6-27.3</sub> reported in literature was confirmed and a new compound  $\tau_2$ -Cu<sub>45.8</sub> Ni<sub>25</sub> Si<sub>29.2</sub> with nearly no homogeneity range was observed. The  $\theta$ -Ni<sub>2</sub>Si compound, which exists above 820  $^{\circ}$ C in the binary Ni–Si system, was found to be stable at 700  $^{\circ}$ C and the composition range of Cu is 12.7–20.6 at.% Cu. The ternary solubilities of binary compounds were measured and noticeably the Cu<sub>56</sub>Si<sub>11</sub> compound can dissolve Ni up to 21.9 at.%.

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# 1. Introduction

The Cu-Ni-Si system is an important system in industry. Typically, the Corson alloys (Cu rich, Cu-Ni-Si-X<sub>(x=none or Mg, Sn, Zn, et al.)</sub> alloy) attracted much attention due to their good balance of high strength, high electrical conductivity and bending formability [1–7]. For example, the Corson alloys C7025 ( $Cu_{96.2}Ni_3Si_{0.65}Mg_{0.15}$ , in wt.%) with high efficiency are widely used for connectors, lead frames and CPU sockets [8]. NKC164E (Cu<sub>98.05</sub>Ni<sub>1.6</sub>Si<sub>0.35</sub>, in wt.%) alloy with high electric conductivity can be used for connectors and wire harness [8]. These Corson alloys feature the age-hardening effect by precipitation of low-temperature Ni<sub>2</sub>Si  $(\delta-Ni_2Si)$  particles or other compounds during heat treatment between 450 °C and 550 °C [9-11]. In addition, the silicon Monel alloys ( $Ni_{62-68}Cu_{28-31}Si_{3.5-4.5}Fe_{<3}Mn_{0.5-1.5}$ , in wt.%) are used for machine parts subjected to friction and operated under special conditions because of their high strength, ductility, corrosion resistance and wear resistance [12]. Knowledge of the phase equilibria on the Cu-Ni-Si system is very significant for development of advanced Cu-Ni-Si alloy. However, information on the phase equilibria of Cu-Ni-Si is very limited.

The Cu-Ni-Si system has been assessed by Jänecke [13], Chang et al. [14] and Drits et al. [15]. Recently, Hari Kumar et al. [16] made

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a critical review of the phase equilibria [1-4,17-30] and thermodynamic properties [31] up to the year 2002. He pointed out that there was a great disagreement among the literature data. The significant discrepancies lie in the solubility of the binary compounds, the solubility of the Fcc\_A1 phase in the Cu rich corner, the existence and stability of ternary compounds and so on. In the following, the phase diagram data are briefly reviewed with emphasis on the data concerning the present experiment. More information was published by Hari Kumar et al. [16]. By means of thermal analysis (TA), metallographic, X-ray diffraction (XRD), dilatometry and hardness measurement, Okamoto [20-23] investigated and reported several isothermal sections in the Cu-rich corner and many vertical sections. A ternary compound  $\tau$  with 12–15 wt.% Si and 11–12 wt.% Ni was reported [22]. This ternary compound is formed by the ternary peritectic reaction Liquid +  $Cu_{56}Si_{11} + \theta$ -Ni<sub>2</sub>Si  $\leftrightarrow \tau$  at 859 °C and can be stable down to 450 °C. Large solubilities of  $\theta$ -Ni<sub>2</sub>Si (20 wt.%), Ni<sub>31</sub>Si<sub>12</sub> (35 wt.%), and Cu<sub>56</sub>Si<sub>11</sub> (25 wt.%) were reported [21,22]. Lashko and Sorokina [26] reported several phase equilibria observed in the Cu-Ni side by examining several alloys and found the solubilities of Ni<sub>3</sub>Si, Ni<sub>31</sub>Si<sub>12</sub> and  $\delta$ -Ni<sub>2</sub>Si are small. Sokolovskaya et al. [27,28] measured the isothermal sections at 500 °C. The ternary compound  $\tau$  found by Okamoto [22] was not observed. The  $\theta$ -Ni<sub>2</sub>Si phase, which is stable above 820 °C in the binary Ni–Si phase diagram, was observed at 500 °C in the ternary system and it can dissolve 10 at.% Cu.

The experimental binary phase diagrams were compiled in Ref. [32]. Table 1 shows the crystallographic data of the phases at 700  $^{\circ}\text{C}$  in the Cu–Ni–Si system. In the Ni–Si system, Ni<sub>3</sub>Si and Ni<sub>3</sub>Si<sub>2</sub> show narrow homogeneity. Only Cu<sub>15</sub>Si<sub>4</sub> has no homogeneity in

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**Table 1**List of the crystallographic data of the phases at 700 °C in the Cu–Ni–Si system.

Phase	Pearson symbol	Space group	Prototype	Lattice parameter	Reference		
				$a/\alpha^a$	$b/eta^{ m a}$	$c/\gamma^{a}$	
Liquid	=	=	_	_	_	_	_
Fcc_A1	cF4	Fm-3m	Cu	3.615(Cu) 3.5238(Ni)			[33]
Si	cF8	Fd-3m	C	5.4309			[34]
Ni <sub>3</sub> Si	cP4	Pm-3m	AuCu <sub>3</sub>	3.506			[35]
Ni <sub>31</sub> Si <sub>12</sub>	hP43	P321	Ni <sub>31</sub> Si <sub>12</sub>	6.667		12.277/120°	[36]
$\delta$ -Ni <sub>2</sub> Si	oP12	Pbnm	Co <sub>2</sub> Si	7.0649	5.0012	3.7307	[37]
$Ni_3Si_2$	oC80	Cmc2 <sub>1</sub>	$Ni_3Si_2$	12.229	10.805	6.924	[38]
$\theta$ -Ni <sub>2</sub> Si <sup>b</sup>	hP4.5	P6 <sub>3</sub> /mmc	$Ni_2In$	3.855		4.952/120°	[39]
NiSi	oP8	Pnma	MnP	5.18	3.34	5.62	[40]
NiSi <sub>2</sub>	cF12	Fm-3m	CaF <sub>2</sub>	5.395			[41]
Cu <sub>7</sub> Si <sup>c</sup>	hP2	P6 <sub>3</sub> /mmc	Mg	2.561		4.184/120°	[37]
Cu <sub>56</sub> Si <sub>11</sub> d	cP19.98	P4 <sub>1</sub> 32	$\beta$ Mn	6.222			[42]
Cu <sub>15</sub> Si <sub>4</sub>	cI76	I-43d	Cu <sub>15</sub> Si <sub>4</sub>	9.714			[43]
Cu <sub>19</sub> Si <sub>6</sub>	oP16	P	_	6.041	6.356	4.288	[37]

- <sup>a</sup> The degrees of the missing  $\alpha$ ,  $\beta$ , and  $\gamma$  angle are  $90^{\circ}$ .
- $^{\text{b}}\,$  The composition is  $\text{Cu}_{0.15}\text{Ni}_{0.5}\text{Si}_{0.35}.$
- <sup>c</sup> The composition is Cu<sub>6.69</sub>Si.
- <sup>d</sup> The composition is Cu<sub>83.3</sub>Si<sub>16.7</sub>.

the Cu–Si system. The present work is intended to measure the isothermal section at  $700\,^{\circ}\text{C}$  to provide phase equilibria data for the Cu–Ni–Si system.

#### 2. Experimental procedure

Thirty ternary alloys were prepared in this work using raw materials of Cu(99.99 wt.%), Ni(99.99 wt.%) and Si(99.9999 wt.%) blocks, with their nominal compositions presented in Table 2 and plotted in Fig. 1. The alloys with weight between 1 and 2 g were prepared by arc melting under high purity argon atmosphere. Encapsulated in evacuated silica tubes with a residual argon pressure of  $10^{-3}$  bar, the alloys were annealed at 700 °C for 30 days or more, followed by water quenching. Since the weight loss of each alloy after arc melting was less than 0.5 wt.%, the alloys were not subjected to chemical analysis.

The phase identification was conducted by means of XRD using Cu K $\alpha$  radiation. After standard metallographic preparation, the alloys were investigated using optical microscopy (Leica DMLP, Germany) and scanning electron microscopy (SEM) equipped with energy dispersive X-ray spectroscopy (EDS) (JSM-6360LV, JEOL, Japan) to determine tie-lines or tie-triangle data. It was found that the nominal

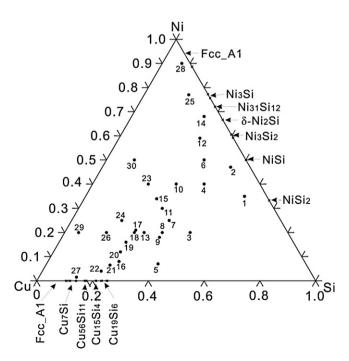


Fig. 1. Nominal alloy composition.

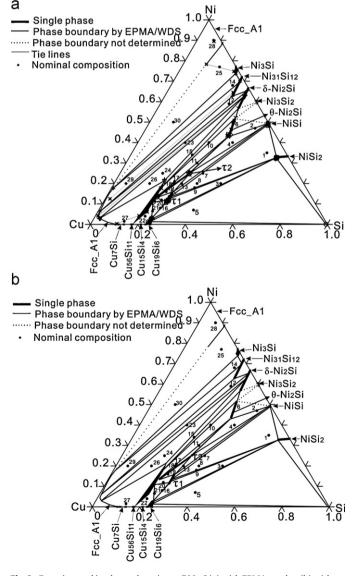


Fig. 2. Experimental isothermal section at 700  $^{\circ}C(a)$  with EPMA results; (b) without EPMA results.

 $\begin{tabular}{ll} \textbf{Table 2} \\ \textbf{Summary of the identified phases, their compositions and lattice parameters for the Cu-Ni-Si alloys annealed at 700 °C.} \\ \end{tabular}$ 

No.	Nominal	Nominal composition (at.%)			Phase composition <sup>b</sup> (at.%)			Lattice parameters (Å) <sup>b</sup>		
	Cu	Ni	Si		Cu	Ni	Si	а	b	c
1	8	35	57	$ au_1$	61.2	11.8	27	-		
				NiSi <sub>2</sub>	5	32.7	62.3	5.405(1)		
				NiSi	0.5	49	50.5	5.183(1)	3.343(2)	5.622(2)
2	7	47	46	NiSi	0.2	49.5	50.3	5.188(1)	3.341(1)	5.622(1)
				$\theta$ -Ni <sub>2</sub> Si	17.4	46.4	36.2	3.889(1)		4.988(2)
3 <sup>c</sup> 35	20	45	$ au_1$	59.8	13.3	26.9	-			
			Cu <sub>19</sub> Si <sub>6</sub>	73	2.7	24.3	6.0156(9)	6.337(9)	4.277(7)	
			NiSi <sub>2</sub>	5.8	32	62.2	5.4021(5)			
4 <sup>c</sup> 20	20	40	40	$ au_2$	45	25.5	29.5	-		
				NiSi	0.7	48.5	50.8	5.184(1)	3.342(2)	5.625(2)
				$\theta$ -Ni <sub>2</sub> Si	19.5	44.5	36	_		
5	53	7	40	Si	0.5	0.1	99.4	5.439(1)		
				NiSi <sub>2</sub>	4.9	32.6	62.5	5.407(1)		
				Cu <sub>19</sub> Si <sub>6</sub>	74.9	1.3	23.8	6.03(1)	6.323(7)	4.288(5)
6	15	50	35	$\theta$ -Ni <sub>2</sub> Si	14.8	49.7	35.5	3.897(3)		4.992(2)
7 <sup>c</sup>	40	25	35	$ au_1$	61.5	11.2	27.3	- ' '		
				NiSi	0.6	49	50.4	5.199(5)	3.347(5)	5.640(6)
8 <sup>c</sup>	45	20	35	$ au_1$	62.3	11.2	26.5	- '	` '	
				NiSi <sub>2</sub>	5.4	32.4	62.2	5.408(1)		
				NiSi	0.8	48.4	50.8	5.198(2)	3.347(2)	5.629(3)
9	47	18	35	$ au_1$	63	10.4	26.6	_	( )	
	••		33	NiSi <sub>2</sub>	5.2	32.6	62.2	5.4043(8)		
				NiSi	0.5	48.9	50.6	5.186(3)	3.349(5)	5.619(7)
0 <sup>c</sup>	30	40	30	Cu <sub>56</sub> Si <sub>11</sub>	61.2	17.7	21.1	6.1771(6)	3.3 15(5)	5,615(7)
Ü	30	10	30	$\theta$ -Ni <sub>2</sub> Si	13.9	50.7	35.4	3.895(2)		4.990(2)
1 <sup>c</sup>	40	30	30	$ au_2$	45.3	25.3	29.4	-		1.550(2)
•	40	30	30	Cu <sub>56</sub> Si <sub>11</sub>	64.6	13.9	21.5	6.189(1)		
				$\theta$ -Ni <sub>2</sub> Si	20.3	43	36.7	3.884(3)		4.991(5)
12 12	59	29	$\delta$ -Ni <sub>2</sub> Si	1.2	65.3	33.5	7.074(2)	5.005(1)	3.7351(9	
2	12	39	29		8.7	62.7	28.6	7.074(2)	3.003(1)	3.7331(3
				Ni <sub>31</sub> Si <sub>12</sub>	93.1	6.1	0.8	2 6171(5)		
2	F1 F	20	20.5	Fcc_A1				3.6171(5)		
.3	51.5	20	28.5	$ au_1$	57.7	15.7	26.6	_		
				τ <sub>2</sub>	46.7	24.6	28.7	-		
	C	CO	26	NiSi	0.4	49.6	50	- 6 600(7)		12.210(7)
14 6	68	26	Ni <sub>31</sub> Si <sub>12</sub>	1.8	69.9	28.3	6.688(7)		12.319(7)	
				Ni <sub>3</sub> Si	1.8	73.8	24.4	3.5107(4)		
	40	2.4	2.0	Fcc_A1	81.4	17.8	0.8	3.6051(6)		
.5 <sup>c</sup>	40	34	26	Cu <sub>56</sub> Si <sub>11</sub>	61.5	17.6	20.9	6.176(1)		
				$\delta$ -Ni <sub>2</sub> Si	9.2	56.7	34.1	-		
		_		$\theta$ -Ni $_2$ Si	12.7	52.1	35.2	3.896(4)		4.991(7)
16	66.5	8	25.5	$ au_1$	61.4	12	26.6	-		
				Cu <sub>19</sub> Si <sub>6</sub>	72.9	3	24.1	6.0258(8)	6.3298(6)	4.2771(4
7	54	21	25	Cu <sub>56</sub> Si <sub>11</sub>	65.2	13.6	21.2	6.1837(4)		
				$\theta$ -Ni <sub>2</sub> Si	20.6	43.4	36	3.893(3)		4.989(6)
8 <sup>c</sup>	55	20	25	$ au_2$	45.7	25	29.3	-		
				$Cu_{56}Si_{11}$	65	13.7	21.3	6.1841(6)		
				$\theta$ -Ni <sub>2</sub> Si	19.2	43.8	37	3.880(3)		4.995(5)
9 <sup>c</sup>	60	16	24	$ au_1$	56.8	16.1	27.1	_		
				$ au_2$	46.1	24.6	29.3	_		
				Cu <sub>56</sub> Si <sub>11</sub>	65.1	13.3	21.6	6.1878(8)		
20	64	12	24	$ au_1$	60	13.2	26.8	-		
				Cu <sub>56</sub> Si <sub>11</sub>	67	11.8	21.2	6.192(1)		
1	70.5	6.5	23	$ au_1$	61.3	11.9	26.8	_		
				Cu <sub>19</sub> Si <sub>6</sub>	72.6	3	24.4	6.023(4)	6.332(2)	4.271(2)
				Cu <sub>56</sub> Si <sub>11</sub>	68.2	10.9	20.9	6.1932(4)	` ,	` ,
.2 <sup>c</sup>	74.9	4	21.1	Cu <sub>19</sub> Si <sub>6</sub>	74.1	1.3	24.6	6.011(5)	6.322(3)	4.276(3)
				Cu <sub>56</sub> Si <sub>11</sub>	73	6.1	20.9	6.2000(3)	(-)	
3c	40	40	20	$\delta$ -Ni <sub>2</sub> Si	2.6	63.7	33.7	7.082(5)	5.004(3)	3.744(2)
	10	10	20	Fcc_A1	94.7	4.2	1.1	3.616(2)	5.661(5)	31, 11(2)
4	57	25	18	Cu <sub>56</sub> Si <sub>11</sub>	57.8	21.9	20.3	6.167(1)		
•	37	23	10	$\delta$ -Ni <sub>2</sub> Si	3.3	63	33.7	7.065(5)	5.015(3)	3.742(2)
				Fcc_A1	94.8	2.9	2.3	3.619(1)	5.015(3)	5.742(2)
25	7	77	16		2		23.2			
J	1	//	10	Ni <sub>3</sub> Si Foc. A1		74.8 78.3		3.521(1)		
06	C E	20	15	Fcc_A1	11.9	78.3	9.8	3.5345(6)		
26	65	20	15	Cu <sub>56</sub> Si <sub>11</sub>	58.1	21.3	20.6	6.1598(8)	F 002(1)	2.7207/
				δ-Ni <sub>2</sub> Si	3.6	62.6	33.8	7.068(2)	5.003(1)	3.7297(8
_	9.5		45 -	Fcc_A1	94.4	3.1	2.5	3.614(2)		
7	85	1.5	13.5	$Cu_{56}Si_{11}$	77.4	4.2	18.4	6.216(1)		
				Fcc_A1	88.7	0.3	11	3.6252(3)		
8	3	90	7	Fcc_A1	3.1	89.5	7.4	3.525(1)		
9 <sup>c</sup>	75	20	5	$Ni_{31}Si_{12}$	7.5	64.5	28	6.694(4)		12.30(1)
				Fcc_A1	85.5	12.5	2	3.609(2)		

Table 2 (Continued)

No.	Nominal composition (at.%)			Phase <sup>a</sup>	Phase cor	nposition <sup>b</sup> (at.%	(at.%) Lattice		e parameters (Å) <sup>b</sup>		
	Cu	Ni	Si		Cu	Ni	Si	a	b	С	
30 <sup>c,d</sup>	40	50	10	Ni <sub>3</sub> Si	3	72.7	24.3	=			
				Fcc_A1	46.6	46.3	7.1	_			

<sup>&</sup>lt;sup>a</sup> The determination of  $\tau_1$  and  $\tau_2$  depends on the comparison between the XRD patterns of the corresponding alloys and EPMA results because there are no standard XRD patterns for  $\tau_1$  and  $\tau_2$ .

compositions of some alloys, whose weight loss after arc melting was negligible, were not in the tie-triangle measured by SEM/EDS. Then, all the alloys were further examined by electron probe microanalysis equipped with wave dispersive X-ray spectroscopy (EPMA/WDS) (JXA-8100, JEOL, Japan) to acquire more accurate data.

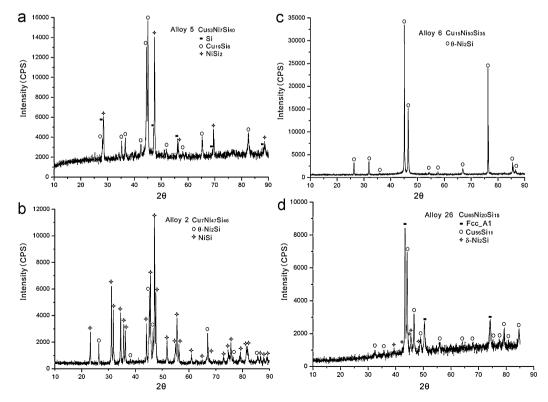
# 3. Experimental result and discussion

The identified phases, their compositions and lattice parameters in the alloys are presented in Table 2. Fig. 2 shows the measured isothermal section at 700 °C. Sixteen alloys are in three-phase regions, so 12 tie-triangles were determined: Cu<sub>19</sub>Si<sub>6</sub>+NiSi<sub>2</sub>+Si, Cu<sub>19</sub>Si<sub>6</sub>+ $\tau_1$ +NiSi<sub>2</sub>,  $\tau_1$ +NiSi+NiSi<sub>2</sub>, Cu<sub>56</sub>Si<sub>11</sub>+ $\tau_1$ +Cu<sub>19</sub>Si<sub>6</sub>,  $\tau_2$ + $\tau_1$ +NiSi, Cu<sub>56</sub>Si<sub>11</sub>+ $\tau_2$ + $\tau_1$ ,  $\tau_2$ + $\theta$ -Ni<sub>2</sub>Si+NiSi, Cu<sub>56</sub>Si<sub>11</sub>+ $\theta$ -Ni<sub>2</sub>Si+ $\tau_2$ , Cu<sub>56</sub>Si<sub>11</sub>+ $\delta$ -Ni<sub>2</sub>Si, Fcc\_A1+ $\delta$ -Ni<sub>2</sub>Si, Fcc\_A1+Ni<sub>31</sub>Si<sub>12</sub>+ $\delta$ -Ni<sub>2</sub>Si, Fcc\_A1+Ni<sub>31</sub>Si<sub>12</sub>. Figs. 3 and 4 show the XRD patterns and microstructure of representative alloys.

The XRD pattern of alloy  $5(Cu_{53}Ni_7Si_{40})$  in Fig. 3a shows this alloy is in  $Cu_{19}Si_6+NiSi_2+Si$  three-phase region, which is in agreement with the microstructure and EPMA result presented in Fig. 4a. Alloys  $3(Cu_{35}Ni_{20}Si_{45})$  and  $21(Cu_{70.5}Ni_{6.5}Si_{23})$  determine the three-phase triangles of  $Cu_{19}Si_6+\tau_1+NiSi_2$  and  $Cu_{56}Si_{11}+Cu_{19}Si_6+\tau_1$ , respectively. Alloys  $1(Cu_8Ni_{35}Si_{57})$ ,  $8(Cu_{45}Ni_{20}Si_{35})$  and  $9(Cu_{47}Ni_{18}Si_{35})$  are all in the  $\tau_1+NiSi+NiSi_2$ 

three-phase region. Alloys 7(Cu<sub>40</sub>Ni<sub>25</sub>Si<sub>35</sub>), 16(Cu<sub>66.5</sub>Ni<sub>8</sub>Si<sub>25.5</sub>),  $20(Cu_{64}Ni_{12}Si_{24})$  and  $22(Cu_{74.9}Ni_4Si_{21.1})$ , which locate in twophase regions, further confirm the determined tie-triangles. Alloys  $13(Cu_{51.5}Ni_{20}Si_{28.5})$ ,  $4(Cu_{20}Ni_{40}Si_{40})$ ,  $19(Cu_{60}Ni_{16}Si_{24})$ ,  $11(Cu_{40}Ni_{30}Si_{30})$  and  $18(Cu_{55}Ni_{20}Si_{25})$  determine the threephase regions of  $\tau_2+\tau_1+\text{NiSi}$ ,  $\tau_2+\theta-\text{Ni}_2\text{Si}+\text{NiSi}$ ,  $\text{Cu}_{56}\text{Si}_{11}+\tau_2+\tau_1$ and  $Cu_{56}Si_{11}+\theta-Ni_2Si+\tau_2$ , respectively. Fig. 4b and c present the microstructure of alloys 9(Cu<sub>47</sub>Ni<sub>18</sub>Si<sub>35</sub>) and 13(Cu<sub>51.5</sub>Ni<sub>20</sub>Si<sub>28.5</sub>) respectively. All the analyses on these alloys reveal two ternary compounds  $\tau_1$  and  $\tau_2$ . The  $\tau_1$  phase has previously been observed by Okamoto [22] below 850°C around  $Cu_{60.9-66.3}Ni_{9.9-11.2}Si_{23.4-28.3}$ . The present EPMA results show that its homogeneity range is Cu<sub>56.8-63</sub>Ni<sub>10.4-16.1</sub>Si<sub>26.6-27.3</sub> at 700 °C. The ternary compound  $\tau_2$  is observed in this work for the first time. The composition of this phase is determined to be almost constant Cu<sub>45.8</sub>Ni<sub>25</sub>Si<sub>29.2</sub> from EPMA analyses on alloys 4, 11, 13, 18 and 19. It should be mentioned that there are no standard XRD patterns for  $\tau_1$  and  $\tau_2$ . The determination of these two phases depends on the comparison between the XRD patterns of the corresponding alloys and EPMA results.

The  $\theta$ -Ni<sub>2</sub>Si phase exists only above 820 °C in the binary Ni–Si system, but can be stabilized down to 500 °C in the Cu–Ni–Si ternary system by dissolving Cu, as observed by Sokolovskaya et al. [28]



**Fig. 3.** XRD patterns for alloys (a)  $5(Cu_{53}Ni_7Si_{40})$ ; (b)  $2(Cu_7Ni_{47}Si_{46})$ ; (c)  $6(Cu_{15}Ni_{50}Si_{35})$ ; (d)  $26(Cu_{65}Ni_{20}Si_{15})$ .

<sup>&</sup>lt;sup>b</sup> For  $\theta$ -Ni<sub>2</sub>Si and Ni<sub>31</sub>Si<sub>12</sub> phases,  $\alpha = \beta = 90^{\circ}$ ,  $\gamma = 120^{\circ}$ , for other phases,  $\alpha = \beta = \gamma = 90^{\circ}$ .

<sup>&</sup>lt;sup>c</sup> These alloys were annealed for 30 days at 700 °C while the others were annealed for 80 days.

<sup>&</sup>lt;sup>d</sup> The result of alloy 30 is deleted in constructing the phase diagram since the microstructure shows the alloy does not reach equilibrium.

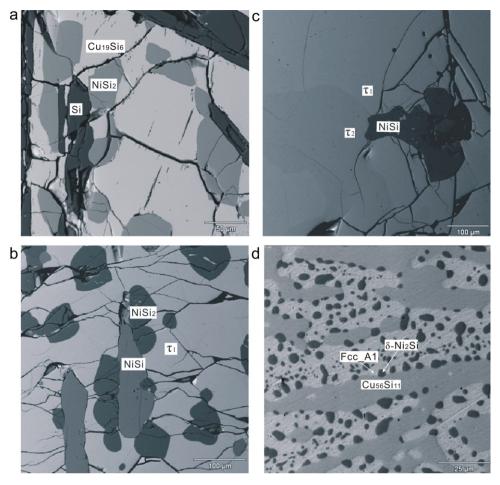


Fig. 4. Back scattered electron images of alloys (a)  $5(Cu_{53}Ni_7Si_{40})$ ; (b)  $9(Cu_{47}Ni_{18}Si_{35})$ ; (c)  $13(Cu_{51.5}Ni_{20}Si_{28.5})$ ; (d)  $26(Cu_{65}Ni_{20}Si_{15})$ .

using XRD. It was corroborated by the present experimental observation, for example, the XRD identification of this phase in the alloys  $2(\text{Cu}_7\text{Ni}_{47}\text{Si}_{46})$  and  $6(\text{Cu}_{15}\text{Ni}_{50}\text{Si}_{35})$  equilibrated at  $700\,^{\circ}\text{C}$  shown in Fig. 3b and c. By substituting Cu for Ni, the  $\theta\text{-Ni}_2\text{Si}$  phase can extend into the ternary system with a solubility of Cu varying from 12.7 to 20.6 at.% at  $700\,^{\circ}\text{C}$ , together with a Si content varying from 35.2 to 37 at.%, which indicates a slight substitution of Si for Ni. The  $\theta\text{-Ni}_2\text{Si}$  phase was identified to be equilibrated with NiSi (alloy 2),  $\tau_2$  (alloys 4, 11, and 18), Cu<sub>56</sub>Si<sub>11</sub> (alloys 10, 11, 15, 17 and 18), and  $\delta\text{-Ni}_2\text{Si}$  (alloy 15).

Alloys  $14(Cu_6Ni_{68}Si_{26})$  and  $12(Cu_{12}Ni_{59}Si_{29})$  are in threephase regions  $Fcc_A1+Ni_3Si+Ni_{31}Si_{12}$  and  $Fcc_A1+Ni_{31}Si_{12}+\delta$ - $Ni_2Si$ , respectively. Alloys  $24(Cu_{57}Ni_{25}Si_{18})$  and  $26(Cu_{65}Ni_{20}Si_{15})$ are in the same three-phase region, Fcc\_A1+ $\delta$ -Ni<sub>2</sub>Si+Cu<sub>56</sub>Si<sub>11</sub>. Figs. 3d and 4d show the XRD pattern and microstructure of alloy 26(Cu<sub>65</sub>Ni<sub>20</sub>Si<sub>15</sub>), respectively. Alloys 29(Cu<sub>75</sub>Ni<sub>20</sub>Si<sub>5</sub>) and 23( $Cu_{40}Ni_{40}Si_{20}$ )) are in two-phase  $Ni_{31}Si_{12}$ +Fcc\_A1 and Fcc\_A1+ $\delta$ -Ni<sub>2</sub>Si regions. The tie-triangles determined by these alloys show agreement with the results of Sokolovskaya et al. [28] at 500 °C. The EPMA result shows that in the copper rich corner, the solubility of Si is decreased to minimum, which means a little addition of Si can cause the precipitation of  $\delta$ -Ni<sub>2</sub>Si or Ni<sub>31</sub>Si<sub>12</sub> compounds from the Fcc\_A1 matrix. This trend can further demonstrate the mechanism of the age-hardening of the Corson alloy although the current experimental temperature is higher than the optimal heat treatment temperature of 450-500 °C.

The  $\text{Cu}_{56}\text{Si}_{11}$  can dissolve a large amount of Ni up to 21.9 at.% mainly by substituting Ni for Cu. At the same time, the Si content also varies slightly with increasing the Ni content. This trend was

previously observed at 500 °C [28]. Fig. 5 shows the lattice parameters of  $\text{Cu}_{56}\text{Si}_{11}$  phase versus Ni content while the Si content is within  $21\pm0.7$  at.%. The lattice parameter decreases as Ni content increases. Such an increase can be explained by the substitution of large Cu atom with smaller Ni atom in  $\text{Cu}_{56}\text{Si}_{11}$  phase.  $\text{Cu}_{19}\text{Si}_{6}$  can dissolve 3 at.% Ni and the Si content remains about 24 at.%. Less than 1 at.% Cu is observed in NiSi compound. NiSi2 can dissolve Cu

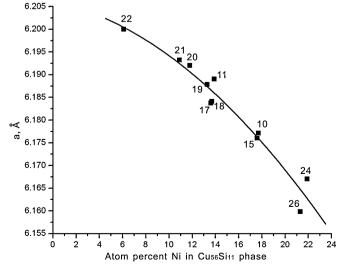


Fig. 5. Lattice parameters of Cu<sub>56</sub>Si<sub>11</sub> phase versus Ni content.

to 5.8 at.%, but Cu substitutes more Si than Ni. In contrast, Cu substitutes much Ni to 9.2 at.% Ni and 8.6 at.% Ni in  $\delta$ -Ni<sub>2</sub>Si and Ni<sub>31</sub>Si<sub>12</sub> respectively, but the Si content remains nearly constant.

## 4. Conclusion

The isothermal section at  $700\,^{\circ}\text{C}$  was determined by XRD, SEM/EDS and EPMA. The existence of the ternary compound  $\tau_1$  is confirmed and it shows a limited homogeneity. A new ternary compound  $\tau_2$  is observed and nearly no homogeneity range was observed. It is corroborated that the  $\theta$ -Ni<sub>2</sub>Si phase can be stabilized by substituting Cu for Ni at low temperatures in the Cu–Ni–Si system. Significant or noticeable solubilities of the third element in the ternary system were observed in the binary compounds Cu<sub>56</sub>Si<sub>11</sub>, Ni<sub>31</sub>Si<sub>12</sub>,  $\delta$ -Ni<sub>2</sub>Si and  $\theta$ -Ni<sub>2</sub>Si at  $700\,^{\circ}$ C.

## Acknowledgements

The financial support from the National Basic Research Program of China (Grant No. 2011CB610401) and the National Natural Science Foundation of China (Grant Nos. 50831007, 51021063 and 50971135) is greatly acknowledged. Mr. Shu Zheng at State Key Lab of Geological Processes and Mineral Resources in China University of Geosciences is acknowledged for help on EPMA analysis.

# References

- [1] M.G. Corson, Z. Metallkd. 19 (1927) 370-371.
- [2] M.G. Corson, Iron Age 119 (1927) 421-424.
- [3] M.G. Corson, Rev. Met. 27 (1930) 194-213.
- [4] M.G. Corson, Rev. Met. 27 (1930) 265-281.
- [5] N. Era, K. Fukamachi, J. Jpn. Res. Inst. Adv. Copper-Base Mater. Technol. 44 (2005) 136–139.
- [6] A. Nishimoto, T. Kamimura, T. Maruyama, K. Nakao, K. Akamatsu, T. Kobayashi, J. Jpn. Res. Inst. Adv. Copper-Base Mater. Technol. 45 (2006) 31–36.
- [7] G. Hagino, H. Eguchi, Y. Takayama, H. Kato, Mater. Sci. Forum 654–656 (2010) 2568–2571.
- $[8]\ http://www.nmm.jx-group.co.jp/english/products/01\_atsuen/03cunisi.htm.$
- [9] M.D. Teplitskii, A.K. Nikolaev, N.I. Revina, V.M. Rozenberg, Fiz. Met. Metalloved. 40 (1975) 1240–1243.
- [10] Y.G. Kim, T.Y. Seong, J.H. Han, J. Mater. Sci. 21 (1986) 1357–1362.

- [11] S.A. Lockyer, F.W. Noble, J. Mater. Sci. 29 (1994) 218–226.
- [12] N.F. Lashko, K.P. Sorokina, A.N. Gorbunov, Metalloved. Term. Obrab. Met. 6 (1966) 48–49.
- [13] E. Jänecke, Brief Handbook of Alloys, Winter, Heidelberg, 1949.
- [14] Y.A. Chang, J.P. Neumann, A. Mikula, D. Goldberg, INCRA Monograph Series 6 Phase Diagrams and Thermodynamic Properties of Ternary Copper–Metal System, NSRD, Washington, 1979.
- [15] M.E. Drits, N.R. Bochvar, L.S. Guzei, E.V. Lysova, N. Padezhnova, L.L. Rokhlin, N.I. Turkina, Binary and Multicomponent Copper-Base Systems, Nauka, Moscow, 1979
- [16] K.C. Hari Kumar, A. Kussmaul, H.L. Lukas, G. Effenberg, Cu-Ni-Si, in: G. Effenberg, S. Ilyenko (Eds.), Materials The Landolt-Börnstein Database, Springer (http://www.springermaterials.com), doi:10.1007/978-3-540-47000-7-33.
- [17] E. Crepaz, Metall. Ital. 23 (1931) 711-716.
- [18] D.G. Jones, L.B. Pfeil, W.T. Griffiths, J. Inst. Met. 46 (1931) 423–442.
- 19] C.H.M. Jenkins, E.H. Bucknell, J. Inst. Met. 57 (1935) 141-189.
- [20] M. Okamoto, J. Jpn. Inst. Met. 2 (1938) 211–232.
- 21] M. Okamoto, J. Jpn. Inst. Met. 3 (1939) 336-348.
- [22] M. Okamoto, J. Jpn. Inst. Met. 3 (1939) 365-402.
- [23] M. Okamoto, J. Jpn. Inst. Met. 3 (1939) 411-420.
- [24] I.I. Novikov, L.I. Dautova, Zh. Neorg. Khim. 2 (1957) 2766-2770.
- [25] I.I. Novikov, L.I. Dautova, Trudy Inst. Yadernoi Fiz., Akad. Nauk Kazakh. SSR 1 (1958) 274–281.
- [26] N.F. Lashko, K.P. Sorokina, Zh. Neorg. Khim. 4 (1959) 1613-1615.
- [27] E.M. Sokolovskaya, O.I. Chechernikova, E.I. Gladyshevskii, O.I. Bodak, Vestn. Mosk. Univ., Ser. 2: Khim. 12 (1971) 446–449.
- [28] E.M. Sokolovskaya, O.I. Chechernikova, E.I. Gladyshevskii, O.I. Bodak, Izv. Akad. Nauk SSSR, Metally 6 (1973) 192–196.
- [29] O.I. Chechernikova, E.M. Sokolovskaya, L.S. Guzei, Vestn. Mosk. Univ., Ser. 2: Khim. 13 (1972) 486–489.
- [30] E. Lugscheider, Proc. 5th Int. Conf. Therm. Anal. (ICTA 5) 9 (1977) 8-101.
- [31] V. Witusiewicz, I. Arpshofen, H. Siefert, F. Sommer, F. Aldinger, Z. Metallkd. 91 (2000) 128–142.
- [32] T.B. Massalski, Binary Alloy Phase Diagrams, second ed., ASM International, Metals Park, OH, 1986.
- [33] H.E. Swanson, E. Tatge, Natl. Bur. Stand. (U.S.) Circ. 539 (1953) 1-95.
- [34] M.C. Morris, H.F. McMurdie, Natl. Bur. Stand. (U.S.) Monogr. 25 (1976) 1–109.
- [35] Y. Oya, T. Suzuki, Z. Metallkd. 74 (1983) 21-24.
- [36] G.S. Saini, L.D. Calvert, J.B. Taylor, Can. J. Chem. 42 (1964) 1511–1517.
- [37] PDF2004, International Centre for Diffraction Data, PA, USA.
- [38] G. Pilstrom, Acta Chem. Scand. 15 (1961) 893–902.
- [39] A. Osawa, M. Okamoto, Sci. Rep. Fac. Sci., Kyushu Univ., Geol. 27 (1939) 326–347
- [40] K. Toman, B. Panenske, V. Odolena, Acta Crystallogr. 4 (1951) 462–464.
- [41] K. Schubert, H. Pfisterer, Z. Metallkd. 41 (1950) 433–441.
- [42] S. Arrhenius, A. Westgren, Z. Phys. Chem. 14 (1931) 66–79.
- [43] F.R. Morral, A. Westgren, Ark. Kemi, Mineral. Geol. 11B (1934) 1–6.